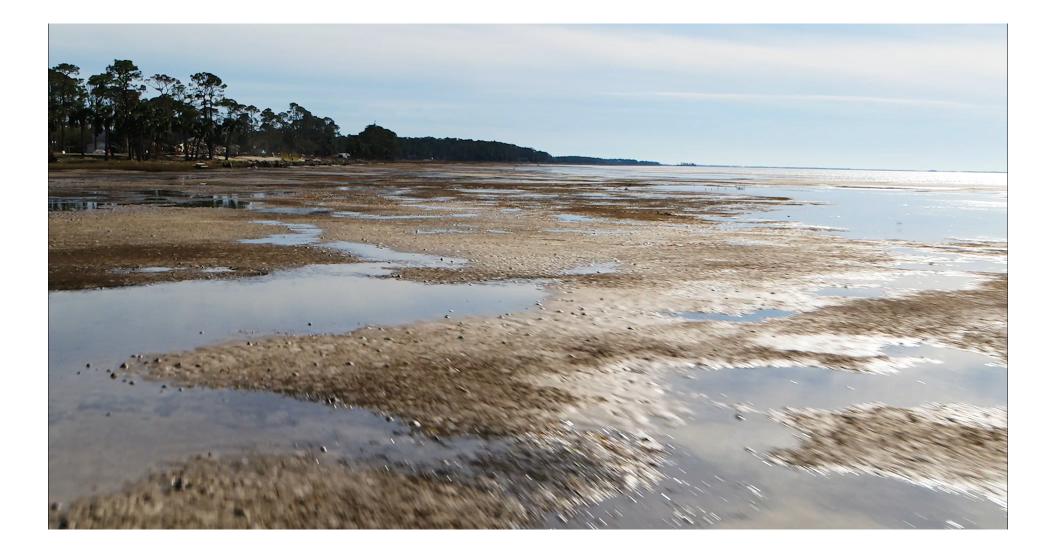
SIMPSON Strong-Tie

Changes in Wind Design With ASCE 7-16

Silvia C Dyer, MS, PE Branch Engineer – Southeast USA





Fundamental Changes in the ASCE 7-16

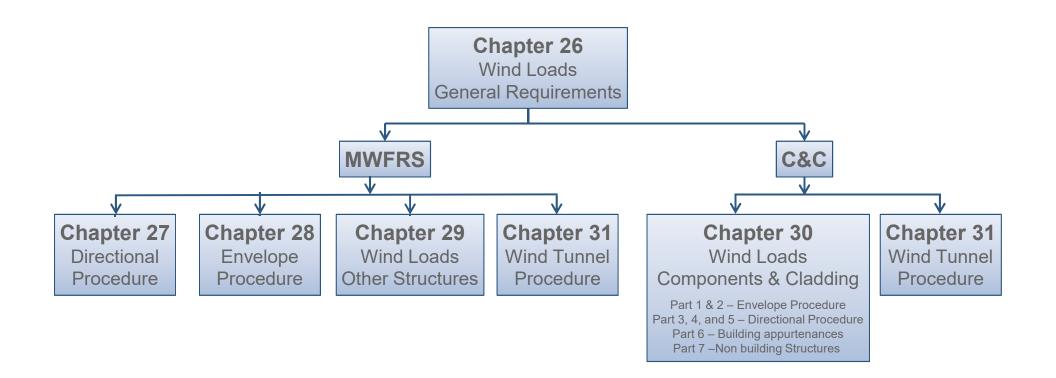
Let's summarize the fundamental changes between ASCE 7-10 and ASCE 7-16



Evolution of the Wind Codes

| Year | Overview | UBC | IBC |
|-----------------|--|------------------|-----------|
| ANSI A58.1-1955 | Initial wind design standard | | - |
| ANSI A58.1-1972 | Quantum Leap in Sophistication, but plagued with ambiguities | 1979 | - |
| ANSI A58.1-1982 | Fixed Issues with 1972 document | 1982, 1985, 1988 | - |
| ASCE7-88 | ASCE took over maintenance of standard with few changes from '82 | 1991, 1994, 1997 | - |
| ASCE7-93 | No Changes Made | - | - |
| ASCE7-95 | Significant update: 3-Second Gusts, topographic effects, wind-induced torsions, simplified procedure for buildings under 60 ft | - | - |
| ASCE7-98 | Wind Speed Map updated, Wind Directionality Factor Added, Exp. C&D definitions changed, procedures defined, glazing protection added | - | 2000 |
| ASCE7-02 | Minor Updates | - | 2003 |
| ASCE7-05 | Surface Roughness Added to help better define Exposure Categories, Other Minor Updates | - | 2006 2009 |
| ASCE7-10 | Wind Map Changes, Reorganization | - | 2012 201 |
| ASCE7-16 | Wind Map changes, new factors, zone changes, tornado guidelines | | 2018 |

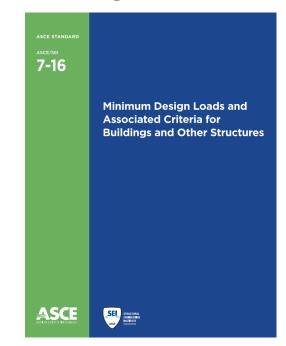
ASCE 7-16 Wind



Changes Pertaining to Wind Loads to ASCE 7-16

The 2016 version of this standard has several significant changes from 2010:

- Enclosure Classification
- Basic Wind Speed
- Ground elevation above Sea Level
- Edge Zones
- Rooftop Equipment
- Design Wind loads: Circular bins, Silos, Tanks
- Wind loads on Rooftop Solar Panels
- Design Wind Pressures Component Cladding Loads on roofs with h <= 60 ft
- Attached canopies on buildings with h <= 60 ft
- Tornado Limitations



Building, Partially Openings – New enclosure classification in ASCE 7-16

| Enclosure Classification | Criteria for Enclosure Classification | Internal Pressure | Internal Pressure Coefficient, (GC_{pi}) |
|------------------------------|--|-------------------|--|
| Enclosed buildings | A_o is less than the smaller of $0.01A_g$ or 4 sq ft (0.37 m) and $A_{oi}/A_{gi} \le 0.2$ | Moderate | +0.18 -0.18 |
| Partially enclosed buildings | $A_o > 1.1 A_{oi}$ and $A_o >$ the lesser of $0.01 A_g$ or 4 sq ft (0.37 m) and $A_{oi}/A_{gi} \le 0.2$ | High | +0.55 -0.55 |
| Partially open buildings | A building that does not comply with Enclosed, Partially Enclosed, or Open classifications | Moderate | +0.18 -0.18 |
| Open buildings | Each wall is at least 80% open | Negligible | 0.00 |

 Table 26.13-1 Main Wind Force Resisting System and Components and Cladding (All Heights): Internal Pressure Coefficient, (GC_{pi}), for

 Enclosed, Partially Enclosed, Partially Open, and Open Buildings (Walls and Roof)

Notes

1. Plus and minus signs signify pressures acting toward and away from the internal surfaces, respectively.

2. Values of (GC_{pi}) shall be used with q_z or q_h as specified.

3. Two cases shall be considered to determine the critical load requirements for the appropriate condition:

a. A positive value of (GC_{pi}) applied to all internal surfaces, or

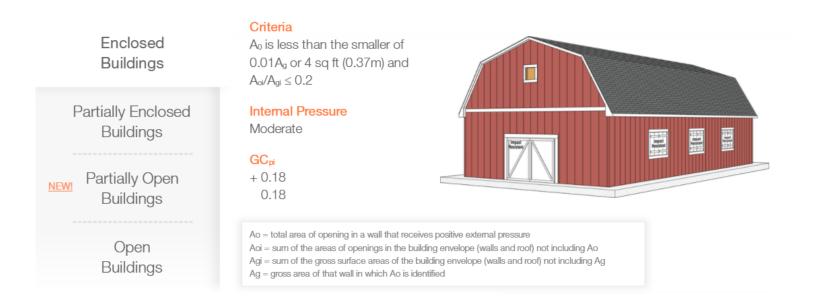
b. A negative value of (GC_{pi}) applied to all internal surfaces.



New

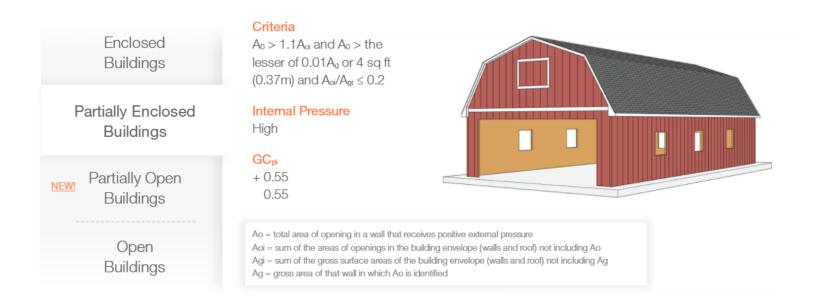
ASCE 7-16 Contains Four Enclosure Classifications

View Table 26.13-1



ASCE 7-16 Contains Four Enclosure Classifications

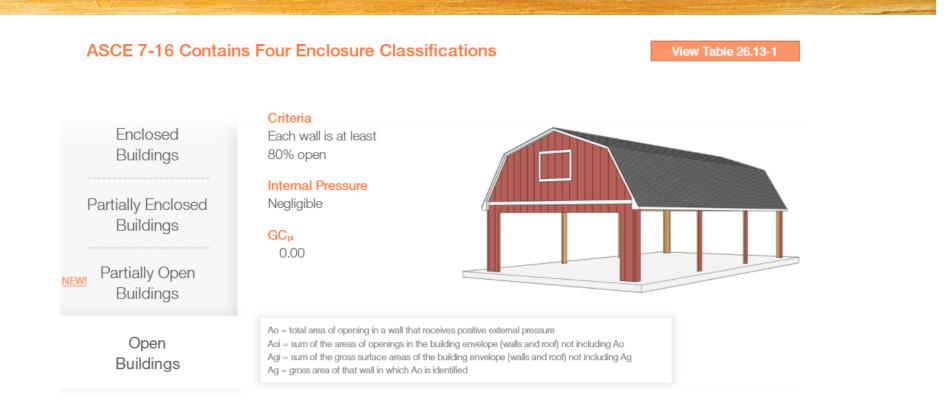
View Table 26.13-1



ASCE 7-16 Contains Four Enclosure Classifications

View Table 26.13-1





Basic Wind Speed

New

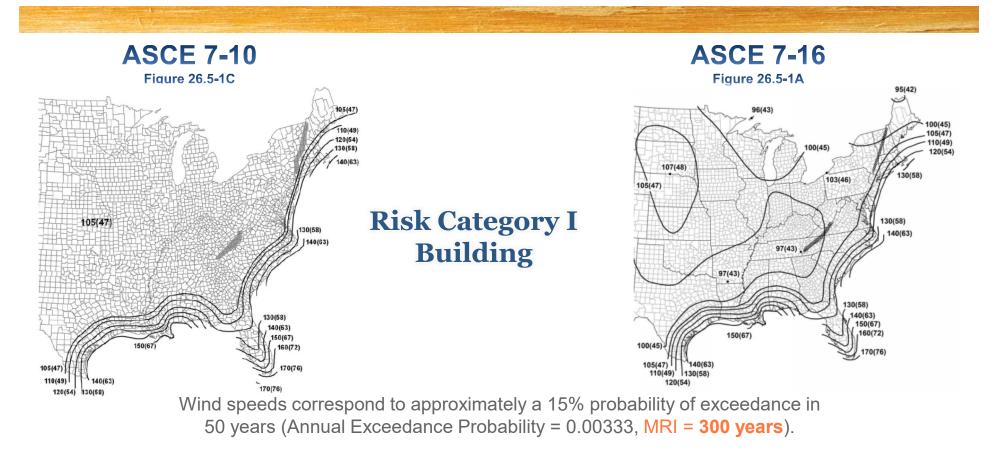
• Basic Wind Speed Maps

R

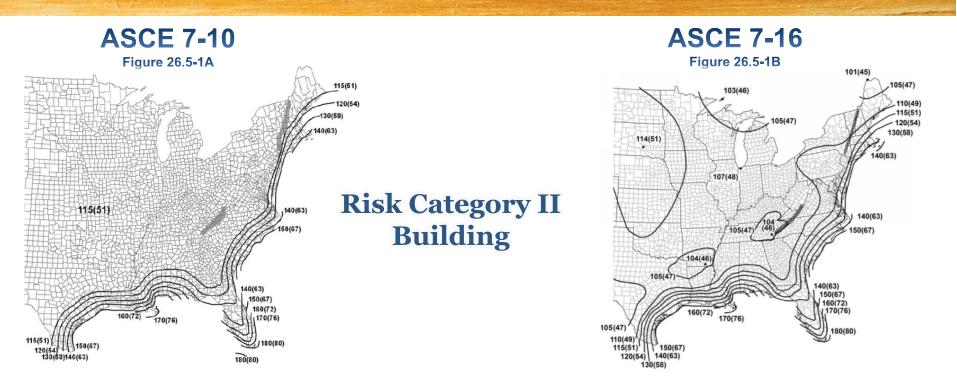
- Maps have been revised outside hurricane prone regions
- Decreased wind speeds outside hurricane prone areas
- Wind Speed Contours have been updated in the Northeast
 - Two updates to the hurricane simulation model used to create the wind maps for ASCE 7-10
 - Decrease of hurricane wind speeds from Virginia to Maine
- New Wind Speed Map for Risk Category IV Buildings

| Building Risk Category | Description | Mean Recurrence Interval |
|---------------------------|---|-----------------------------|
| I | Low hazard to human life in case of failure | 300 years |
| | Most Residential and Commercial Dwellings | 700 years |
| 111 | Substantial risk to human life in case of failure | 1,700 years |
| IV | Essential Facilities | 3,000 years |

Updated Wind Speed Maps



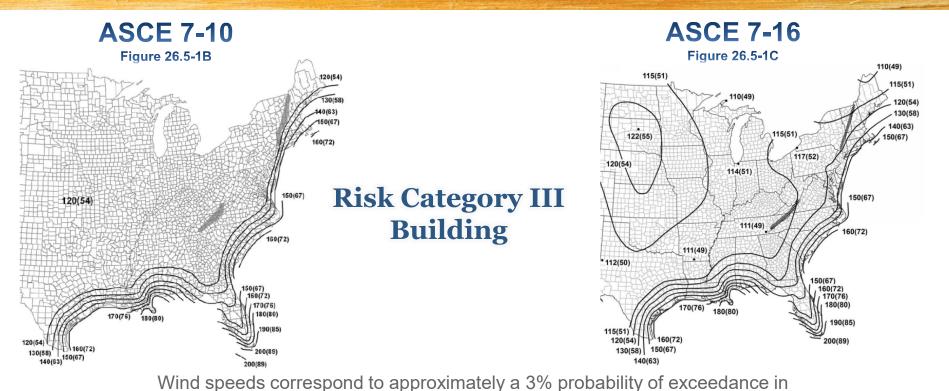
Updated Wind Speed Maps



Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (Annual Exceedance Probability = 0.00143, MRI = **700 years**).

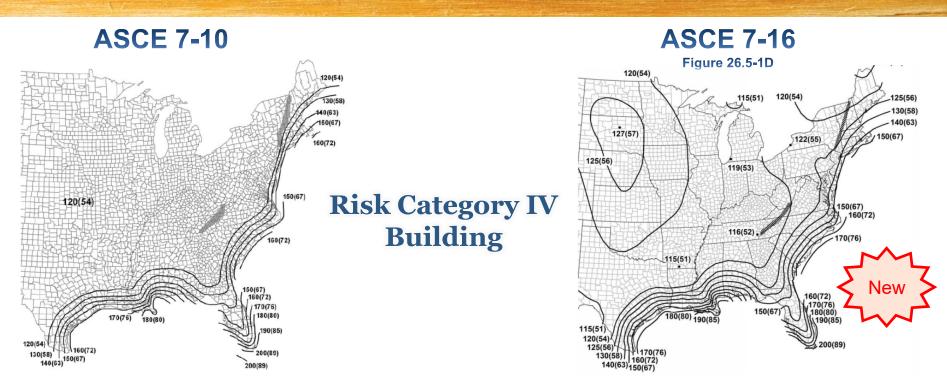
R

Updated Wind Speed Maps



50 years (Annual Exceedance Probability = 0.000588, MRI = **1700 years**).

New Wind Speed Maps



Wind speeds correspond to approximately a 1.6% probability of exceedance in 50 years (Annual Exceedance Probability = 0.000333, MRI = **3000 years**).

Ground Elevation Above Sea Level

 $q_{z} = 0.00256 \text{ K}_{z} \text{ K}_{zt} \text{ K}_{d} \text{ K}_{e} \text{V}^{2} (\text{lb/ft}^{2})$ (26.10-1)

 K_{z} = velocity pressure exposure coefficient

 K_{zt} = topographic factor

 K_d = wind directionality factor K_e = Ground Elevation Factor

 q_z = velocity pressure at height z (lb/ft2)

V = velocity in mi/hour



Source: Significant Changes to the Minimum Design Load Provisions of ASCE 7-16 (ICC publication)

New

Ground Elevation Above Sea Level

$$q_z = 0.00256 K_z K_{zt} K_d K_e V^2 (Ib/ft^2) (26.10-1)$$

 $P = \frac{1}{2} \rho V^2$

Mass density at air standard atmosphere = 0.002378 lb-s²/ft⁴ (slug/ft³)

$$P = \frac{1}{2} (0.002378 \text{ Ib-s}^2/\text{ft}^4) (V \underset{\text{hour}}{\text{mi}} X \frac{5280 \text{ ft}}{1 \text{ mi}} X \frac{1 \text{hour}}{3600 \text{s}})^2$$

 $P = 0.00256 V^2$

Source: Significant Changes to the Minimum Design Load Provisions of ASCE 7-16 (ICC publication)

Ground Elevation Above Sea Level

Table 26.9-1 Ground Elevation Factor, K_e

| Ground Elevation above Sea Level | | Ground Elevation | |
|----------------------------------|--------|--------------------------------|--|
| ft | m | Factor <i>K_e</i> | |
| <0 | <0 | See note 2 | |
| 0 | 0 | 1.00 | |
| 1,000 | 305 | 0.96 | |
| 2,000 | 610 | 0.93 | |
| 3,000 | 914 | 0.90 | |
| 4,000 | 1,219 | 0.86 | |
| 5,000 | 1,524 | 0.83 | |
| 6,000 | 1,829 | 0.80 | |
| >6,000 | >1,829 | See note 2 | |

Notes

- 1. The conservative approximation K_e 1.00 is permitted in all cases.
- 2. The factor K_e shall be determined from the above table using interpolation or from the following formula for all elevations:
 - $K_e e^{-0.0000362z_g}$ (z_g ground elevation above sea level in ft).
 - $K_e e^{-0.000119z_g}$ (z_g ground elevation above sea level in m).
- 3. K_e is permitted to be take as 1.00 in all cases.



18% reduction in design wind pressure



Edge Zone Width (a)

Chapter 28

Wind Loads of Buildings: Main Wind Force Resisting System (Envelope Procedure)

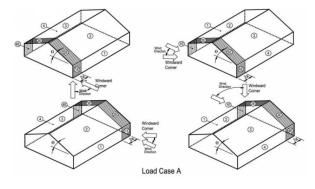
Part 1: Enclosed and Partially Enclosed Low-Rise Buildings Part 2: Enclosed Simple Diaphragm Low-Rise Buildings

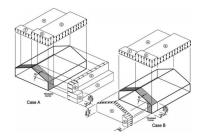
Figures for External Pressure Coefficient (GC_p)

Dimension a = 10% of least horizontal dimension or 0.4*h*, whichever is smaller, but not less than either 4% of least horizontal dimension or 3 ft

Exception: For buildings with Θ - 0 to 7° slope and a least horizontal dimension greater than 300ft, dimension *a* shall be limited to a maximum of 0.8*h*







Edge Zone Width (*a*)

Chapter 30

Wind Loads: Components and Cladding

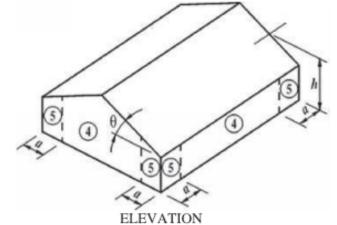
Part 1: Low-Rise Buildings (Envelope Procedure)Part 2: Low-Rise Buildings (Simplified Envelope Procedure)

Figure 30.3-1 External Pressure Coefficient – (GC_p) (walls)

Dimension a = 10% of least horizontal dimension or 0.4*h*, whichever is smaller, but not less than either 4% of least horizontal dimension or 3 ft

Exception: For buildings with Θ - 0 to 7° slope and a least horizontal dimension greater than 300ft, dimension *a* shall be limited to a maximum of 0.8*h*





Rooftop Equipment

Section 29.4.1 has provisions for wind loads for rooftop equipment in buildings of all heights.

Section 26.10.2 gives direction specific on what basic wind speed to use in determining wind loads in roof structures including rooftop equipment **26.10.2 Velocity Pressure.** Velocity pressure, q_z , evaluated at height *z* above ground shall be calculated by the following equation:

 $q_z = 0.00256K_z K_{zl} K_d K_e V^2 (lb/ft^2); V \text{ in mi/h}$ (26.10 1)

 $q_z = 0.613 K_z K_{zt} K_d K_e V^2 (N/m^2); V \text{ in m/s}$ (26.10 1.si)

where

 K_z = velocity pressure exposure coefficient, see Section 26.10.1.

 K_{zt} = topographic factor, see Section 26.8.2.

 K_d = wind directionality factor, see Section 26.6.

 K_e = ground elevation factor, see Section 26.9.

V = basic wind speed, see Section 26.5.

 q_z = velocity pressure at height z.

The velocity pressure at mean roof height is computed as $q_h = q_z$ evaluated from Eq. (26.10 1) using K_z at mean roof height *h*.

The basic wind speed, *V*, used in determination of design wind loads on rooftop structures, rooftop equipment, and other building appurtenances shall consider the Risk Category equal to the greater of the following:

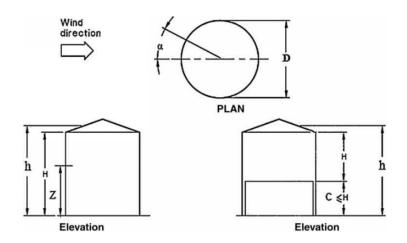
- 1. Risk Category for the building on which the equipment or appurtenance is located or
- 2. Risk Category for any facility to which the equipment or appurtenance provides a necessary service.

Circular Bins, Silos, and Tanks

Section 29.4.2 has provisions for wind loads for circular bins, silos and tanks.

Section 30.12 has provisions for wind loads for components and cladding of circular bins, silos and tanks

$h \leq 120$ ft, $D \leq 120$ ft, and $0.25 \leq H/D \leq 4$







| Section 29.4.3 has provisions for wind loads for rooftop solar panels for buildings of all heights with a flat roof or gable or hip roofs with slopes less than 7°. | Limited to 35° tilt with respect to the roof Low height ≤ 2 ft High height ≤ 4 ft Min gap of $\frac{1}{4}''$ Maximum panel chord length of 6.7 ft |
|--|---|
| Section 29.4.4 has provisions for wind loads for parallel rooftop solar panels for buildings of all heights and roof slopes | Limited to 2° tilt with respect to the roof Max height above roof \leq 10 in. Min gap of 1/4" Maximum panel spacing of 6.7 ft |
| Section 30.13 has provisions for wind loads for rooftop solar panels for non-building structures of all heights with a flat roof or gable or hip roofs with slopes less than 7°. – references back to Section 29.4.3 | Limited to 35° tilt with respect to the roof Low height ≤ 2 ft High height ≤ 4 ft Min gap of $\frac{1}{4}''$ Maximum panel chord length of 6.7 ft |

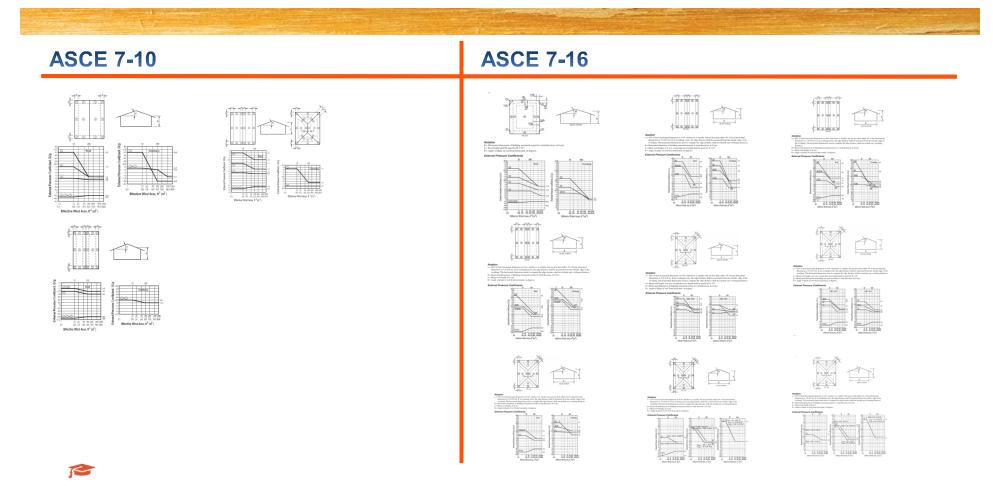
R

| Chapter 30 – Wind Loads – Componer | nts and Cladding (C&C) | | |
|---|---|--|--|
| ASCE 7-10 | ASCE 7-16 | | |
| Part 1 – Enclosed and partially enclosed low-rise buildings with h ≤ 60 ft (18.3m) | Part 1 – Enclosed and partially enclosed low-rise buildings with h ≤ 60 ft (18.3m) | | |
| Part 2 – Simplified approach for enclosed low-rise buildings with h ≤ 60 ft (18.3m) | Part 2 – Simplified approach for enclosed low-rise buildings with h ≤ 60 ft (18.3m) | | |
| Part 3 – Enclosed and partially enclosed for buildings with h > 60 ft(18.3m) | Part 3 – Enclosed and partially enclosed for buildings with h > 60 ft(18.3m) | | |
| Part 4 – Simplified approach for enclosed buildings with h ≤ 160 ft Part 5 – Open buildings for all heights Part 6 – Building appurtenances such as roof | Part 4 – Simplified approach for enclosed buildings with h ≤ 160 ft Part 5 – Open buildings for all heights Part 6 – Building appurtenances such as roof overhangs, parapets, and rooftop equipment | | |
| overhangs, parapets, and rooftop equipment | Part 7 – Non Building structures circular bins, silos and tanks ≤ 120ft and rooftop solar panels for all building heights with flat roofs or gable or hip roofs with roof slopes less than or equal to 7 degrees. | | |

Part 1 and 2 of Chapter 30 - Roof Component and Cladding Pressure Coefficient (GCp) for Enclosed and Partially Enclosed building with $h \le 60$ ft

| ASCE 7-10 | ASCE 7-16 Figures 30.3 2A – I | |
|---|--|--|
| Figures 30.4 2A – C | | |
| A – Gable roofs and overhangs $\Theta \le 7^{\circ}$ B – Gable / Hip roofs $7^{\circ} < \Theta \le 27^{\circ}$ C – Gable Roofs $27^{\circ} < \Theta \le 45^{\circ}$ | A – Gable roofs and overhangs $\Theta \le 7^{\circ}$ B – Gable roofs $7^{\circ} < \Theta \le 20^{\circ}$ C – Gable Roofs $20^{\circ} < \Theta \le 27^{\circ}$ D – Gable Roofs $27^{\circ} < \Theta \le 45^{\circ}$ E – Hip Roofs $7^{\circ} < \Theta \le 20^{\circ}$ F – Hip Roofs overhang $7^{\circ} < \Theta \le 20^{\circ}$ G – Hip Roofs and overhang $20^{\circ} < \Theta \le 27^{\circ}$ H – Hip Roofs $27^{\circ} < \Theta \le 45^{\circ}$ I – Hip Roofs overhang $27^{\circ} < \Theta \le 45^{\circ}$ | |
| | | |

R



| Location | ASCE 7-10 Design Wind Speed (mph) ¹ | ASCE 7-16 Design Wind Speed (mph) ² | Elevation (feet above sea level) ³ | Roof Shape (Gable/Hip) | ASCE 7-10 pressures (psf) | ASCE 7-16 pressures (psf) |
|----------------|--|--|---|---------------------------|---------------------------------|---------------------------------|
| Boston, MA | 129 | 120 | 23 | Gable | -47.7 | -47.8 |
| Doston, IVIA | 129 | 120 | 23 | Hip | -47.7 | -38.9 |
| Miami, FL | 171 | 160 | 7 | Gable | -83.7 | -94.9 |
| Ivnami, FL | 1/1 | 169 | / | Hip | -83.7 | -77.2 |
| Houston, TX | 138 | 136 | 47 | Gable | -54.5 | -61.4 |
| Houston, 1 A | 138 | 130 | 4/ | Hip | -54.5 | -49.9 |
| Pittsburgh, | 115 | 110 | 7(5 | Gable | -37.9 | -39.1 |
| PA | 115 | 110 | 765 | Hip | -37.9 | -31.8 |
| Denver, CO | 1154 | 107 | 5020 | Gable | -37.9 | -31.5 |
| Denver, CO | 115 | 107 | 5232 | Hip | -37.9 | -25.6 |
| Oklahoma | 115 | 109 | 1200 | Gable | -37.9 | -37.8 |
| City, OK | 115 | 109 | 1200 | Hip | -37.9 | -30.8 |
| Spokane, WA | 110 | 102 | 1000 | Gable | -34.6 | -32.3 |
| Spokane, wA | 110 | 102 | 1909 Hip | -34.6 | -26.3 | |
| San Francisco, | 110 | 02 | 5.2 | Gable | -34.6 | -28.1 |
| CA | 110 | 92 | 53 | Hip | -34.6 | -22.8 |
| Des Moines, | 115 | 110 | 800 | Gable | -37.9 | -39.1 |
| IA | 115 | 110 | 800 | Hip | -37.9 | -31.8 |
| Salt Lake | 115 | 102 | 42(1 | Gable | -37.9 | -30.2 |
| City, UT | 115 | 103 | 4261 | Hip | -37.9 | -24.6 |

Wind Pressure Summary Table

Parameters:

- Zone 2 or 2r
- Exposure B
- 15 feet above grade
- Using location elevation factor K_e
- Using smallest applicable EWA (Effective Wind Area)
- Reduced wind speeds from new maps as appropriate



Attached Flat Canopies on Buildings with $h \le 60$ ft

Section 30.11 has provisions for wind loads for attached canopies on buildings with $h \le 60$ ft and a maximum 2% horizontal slope

Figures 30.11-1A and 1B has pressure coefficients for both separate surfaces of attached canopies and considering simultaneous contributions from upper and lower surfaces respectively







Attached Canopies on Buildings with $h \le 60$ ft

Figure 30.11-1A

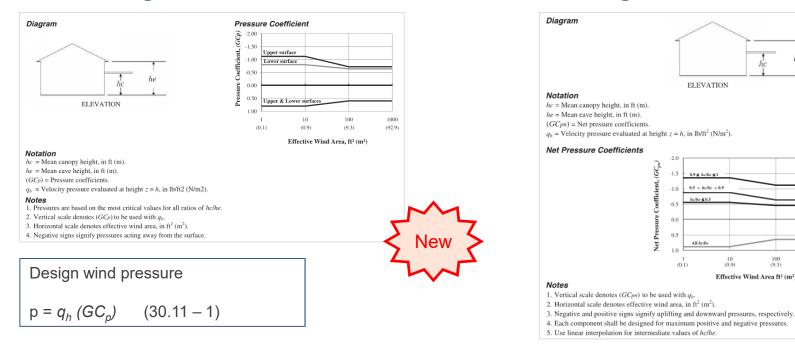


Figure 30.11-1B

-2.0

-1.5

-1.0

-0.5

(GC_{pn})

Coefficient

ure 0.0

Net Press 0.5 ELEVATION

 $0.9 \leq hc/he \leq$

hc/he ≤0.5

All hc/he 1.0

(0.1)

10 (0.9)

100 (9.3)

Effective Wind Area ft2 (m2)

1000 (92.9)

0.5 < hc/he < 0.9

Section C26.14 has provisions providing guidance for designing buildings for tornadoes.



- 1. Tornado wind speeds and probability
- 2. Wind pressures induced by tornadoes vs. other windstorms
- 3. Designing for occupant protection
- 4. Designing to minimize building damage
- 5. Design to maintain continuity of building operations
- 6. Designing trussed communication towers for wind-borne debris



1 – Tornado Wind Speeds and Probability (Section C26.14.1)

Tornado-related winds have a significantly lower probability of occurrence at a specific location than the high winds associated with meteorological events (frontal systems, thunderstorms, and hurricane winds) responsible for the basic wind speeds given in ASCE 7.



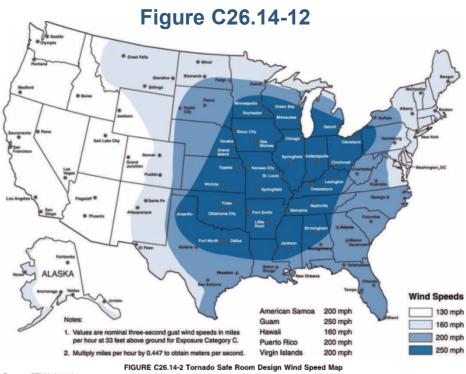
| EF Number | Wind Speed (mph) | (m/s) |
|-----------|------------------|-------|
| EFO | 65 85 | 29 38 |
| EF1 | 86 110 | 39 49 |
| EF2 | 111 135 | 50 60 |
| EF3 | 136 165 | 61 73 |
| EF4 | 166 200 | 74 89 |
| EF5 | >200 | >89 |

Table C26.14-1 Enhanced Fujita (EF) Scale

| EF Number | MRI (Mean Recurrence Interval) |
|-----------|-----------------------------------|
| EF0 – EF1 | 4,000 year MRI |
| EF4 – EF5 | 10,000,000 year MRI |

Note: Speeds are for 3 s peak gust, Exposure C, 33 ft (10 m) above grade. Conversion of mph to $m/s:mph \times 0.44704$ m/s.

Source: NOAA (http://www.spc.noaa.gov/efscale/ef scale.html).





Source: FEMA (2008)

2 – Wind Pressures Induced by Tornadoes Vs. Other Windstorms (Section C26.14.2)

Tornado wind-borne debris shed from buildings indicates that tornado debris has a greater vertical trajectory than hurricane debris. Updrafts are greater in tornadoes than in other windstorms.

New



Photo of Dallas Fire Station #41 courtesy of MSN 2019, DALLAS FIRE-RESCURE/HANDOUT/EPA-EFE/Shutterstock – also found in NSF StEER Event Briefing from Dallas, TX 10/20/2019 EF-3 Tornado

| | S No |
|---|--|
| 3 – Designing for occupant protection | ICC 500 residential and community storm shelters |
| (Section C26.14.3) | FEMA P 320 – prescriptive solutions for residential and small business safe rooms up to 16 occupants |
| | FEMA P 361 – residential and community safe rooms and design and construction QA. |
| 5 – Design to maintain continuity of building operations (Section C26.14.5) | FEMA P 908 – designing a building to ensure that it will remain operational if struck by an EF4or EF5 rated tornado |
| 6 – Designing trussed communication towers for wind borne debris (Section C26.14.6) | FEMA 2012 – minimum design for 40 ft ² of projected surface area of clinging debris at mid height of the tower or 50 ft. |

4 – Designing to minimize building damage (Section 26.14.4)

Two methods:

- 1. Extended method: modified wind pressure calculation parameters then the design wind pressure can simply be calculated using the normal equations in ASCE 7
- 2. Simplified method: combines all parameters into a TF factor



Tornado Limitations in Commentary

Extended method:

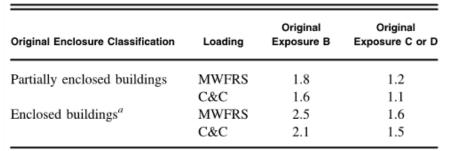
- Wind Speed V: Design for the upper range wind speed within the target EF scale.
- K_z: The velocity pressure exposure coefficient should be based on Exposure Category C
- Directionality K_d : The directionality factor should be taken as 1.0
- Topography K_{zt}: The topographic factor should be taken as 1.0
- Gust effect factor, G: The gust effect factor should be taken as 0.90 or higher if appropriate
- Internal pressure GC_{pi} : The internal pressure coefficient should be taken as ± 0.55
- Velocity pressure q: The velocity pressure should be determined at mean roof height, q_h
- MWFRS C_p: Pressures on the MWFRS should be based on the pressure coefficient, CP specified for the directional procedure in Chapter 27
- C&C, GC_p values: the pressure coefficients, GC_p, for components and cladding are permitted to be reduced by 10%



Tornado Limitations in Commentary

Simplified method:

Table C26.14-4 Increases in Design Loads to Address Tornado Risks Using Recommended Tornado Factors



^{*a*}The tornado factors to be used to increase the design loads on elements of enclosed buildings are based on the effects of high internal pressures. High internal pressures have a much greater effect on elements that typically receive less wind, so the net effect of these increase factors is typically much higher than would result if the building were designed for the specific tornado loads or if the tornado factors for partially enclosed buildings were used with partially enclosed building designs.

$$p_{tornado} = p_{design} (V_{tornado} / V_{design})^2 TF$$



Recap

Changes in the 2016 edition of the ASCE 7 include:



Wind maps modified to include more data. New Risk Category map, all maps include interior basic wind velocities.



Component and cladding GC_p information include more data. Zones increased, more maps to include hip roofs. Overall increase in external pressure coefficient



New elevation factor K_e to be included in the velocity pressure formula q to account the drop in pressure as site elevation increases with respect to sea level



New wind loads specific to silos, tanks, solar panels, canopies attached to buildings



Modifications to roof top equipment parameters

Guidelines for tornado design available in the commentary



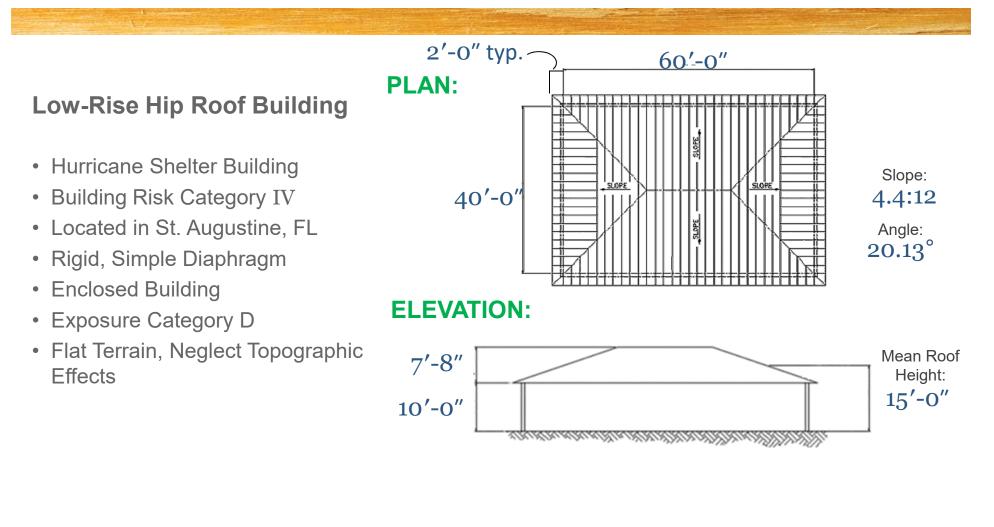


Design Example: C&C Low-Rise Buildings (Simplified) Procedures (2010 vs. 2016)

Let's compare the differences in low-rise building simplified wind pressure calculation procedures between ASCE 7-2010 and ASCE 7-2016



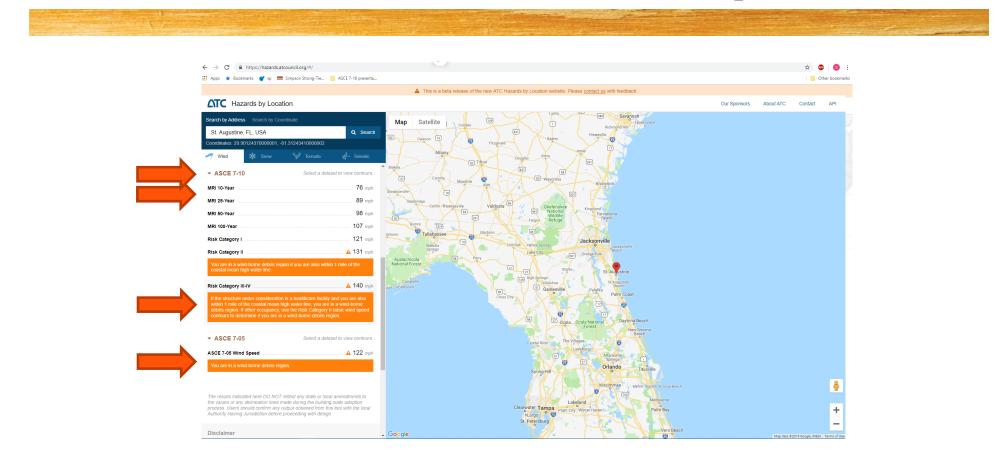
The Problem Statement



Simplified Procedure Overview

| | Steps | ASCE 7-16 Ref. | ASCE 7-10 Ref. |
|---|---|--|---|
| 1 | Verify building general requirements and conditions to use this method | Sections 30.4 and 30.4.1 | Sections 30.5 and 30.5.1 |
| 2 | Establish building Risk Category | Table 1.5-1 | Table 1.5-1 |
| 3 | Determine Basic Wind Speed | Figure 26.5-1D | Figure 26.5-1B |
| 4 | Determine Wind load Parameters (Exposure Category and Topographic factor K_{zt}) | Sections 26.7, 26.8 and Figure 26.8-1 | Section 26.7, 26.8 and Figure 26.8-1 |
| 5 | Select Simplified Design Wind Pressure (p _{S30}) | Figure 30.4-1 | Figure 30.5-1 |
| 6 | Select Height and Exposure Coefficient (λ) | Figure 30.4-1 | Figure 30.5-1 |
| 7 | Calculate Adjusted Wind Pressure (<i>p</i> _{net}) | Equation 30.4-1 | Equation 30.5-1 |

Alternative Method for Basic Wind Speed



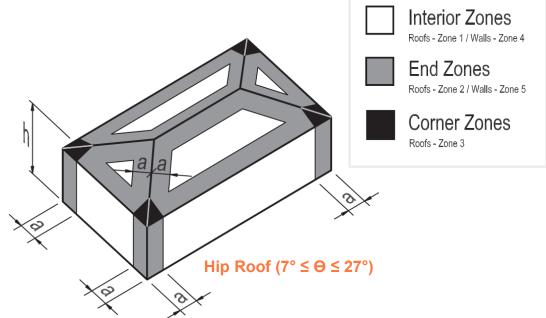
Available at hazards.atcouncil.org

Note 3:

For hip roofs with $\Theta \le 25^{\circ}$, Zone 3 shall be treated as Zone 2

Note 5:

a: 10% of least horizontal dimension or .4h, whichever is smaller but not less than either 4% of least horizontal dimension or 3 ft



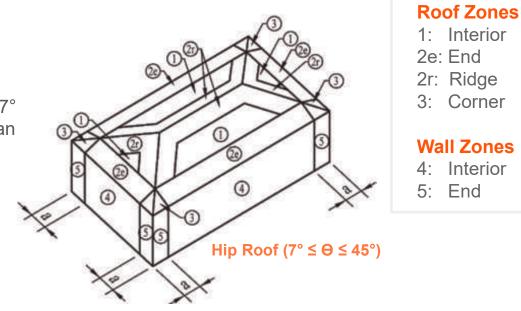
a = 4'-0"

(Figure 30.5-1 ASCE 7-10) Components and Cladding, Part 2 [h ≤ 60ft (h ≤ 18.3m)]: Design Wind Pressure for Enclosed Buildings – Walls and Roofs

Notation: a = 10% of least horizontal dimension or .4h, whichever is smaller but not less than either 4% of least horizontal dimension or 3 ft

Exception: for buildings with Angle = 0° to 7° and a least horizontal dimension greater than 300 ft, dimension a shall be limited to a maximum of 0.8h

Note 3: For hip roofs with $\Theta \leq 25^{\circ}$, Zone 3 shall be treated as Zone 2e and 2r.



1: Interior

- 3: Corner

Wall Zones

- 4. Interior
- 5: End

a = 4' - 0''

(Figure 30.4-1 ASCE 7-16) Components and Cladding, Part 2 [$h \le 60$ ft ($h \le 18.3$ m)]: Design Wind Pressure for Enclosed Buildings - Walls and Roofs

Simplified Procedure Exposure Coefficient

Find the Exposure Coefficient

- Mean roof height = 15 ft
- Exposure Category D
- Exposure Coefficient = 1.47

| | | ent Factor | | | | | | | | | |
|-------------|------------|------------|----------------|--|--|--|--|--|--|--|--|
| for Build | ling Heign | t and Expo | sure, A | | | | | | | | |
| Mean roof | Exposure | | | | | | | | | | |
| height (ft) | B | C | D | | | | | | | | |
| 15 | 1.00 | 1.21 | 1.47 | | | | | | | | |
| 20 | 1.00 | 1.29 | 1.55 | | | | | | | | |
| 25 | 1.00 | 1.35 | 1.61 | | | | | | | | |
| 30 | 1.00 | 1.40 | 1.66 | | | | | | | | |
| 35 | 1.05 | 1.45 | 1.70 | | | | | | | | |
| 40 | 1.09 | 1.49 | 1.74 | | | | | | | | |
| 45 | 1.12 | 1.53 | 1.78 | | | | | | | | |
| 50 | 1.16 | 1.56 | 1.81 | | | | | | | | |
| 55 | 1.19 | 1.59 | 1.84 | | | | | | | | |
| 60 | 1.22 | 1.62 | 1.87 | | | | | | | | |

Figure 30.4-1 ASCE 7-16 or Figure 30.5-1 ASCE 7-10

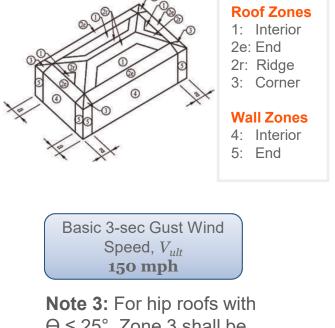
| | Cor | nponen | ts and | l Cla | Iding | - M | ethod | 11 | | | | | | | | h < | 60 ft | | | |
|-------------|----------|-------------|----------|-------|--------------|----------------|-------|-------|------|--------------------|------|------------|--------------|----------------|--------------|---------|-------|------------------|------|------------------|
| ig | | 0.5-1 (c | | | | | | | Pres | sures | | | | | N. | | | | | |
| | Enc | losed B | uildiı | ngs | | | | | | | | | | | wai | IS & | z Ro | 015 | | |
| | | | , | |)osio | m W | ind I | Proc | suro | , p _{net} | (n | ef) /F | VDOS | uro R | ot h - | 20.8 | , | | | |
| | L | Effective | <u> </u> | ICI L | rearg | | inu i | 163 | | | | | | | at 11 - | - 30 n. | / | | | |
| | Zon | e wind area | | 10 | 4 | 15 | 4 | 20 | | sic W 30 | _ | peed 40 | <u> </u> | on) 50 | 4 | 60 | 4 | 30 | 20 | |
| | 1 | 10 | 12.5 | -19.9 | 13.7 | | _ | | | -27.8 | | 1.000 | 23.3 | | 26.5 | | | | _ | -65.9 |
| | | 20 | 11.4 | -19.9 | 12.5 | | | | _ | | 18.5 | -31.4 | 4 | -36.0 | 20.5 | -41.0 | | -51.9 | | -64.0 |
| 8 | 1 | 50 | 10.0 | -18.6 | 10.9 | | | _ | | _ | 16.1 | -30.2 | _ | -34.6 | 21.1 | -39.4 | 26.7 | -49.9 | 32.9 | -61.6 |
| | 1 | 100 | 8.9 | -18.1 | 9.7 | -19.8 | 10.5 | -21.5 | 12.4 | -25.2 | 14.3 | -29.3 | 16.5 | -33.6 | 18.7 | -38.2 | 23.7 | -48.4 | 29.3 | -59.8 |
| | 2 | 10 | 12.5 | -34.7 | 13.7 | | _ | -41.3 | _ | | 20.3 | -56.2 | 23.3 | -64.5 | 26.5 | -73.4 | _ | -92.9 | | 114.6 |
| | 2 | 20 | 11.4 | -31.9 | 12.5 | -34.9 | | _ | | - | | -51.7 | | -59.3 | 24.2 | -67.5 | | -85.4 | | 105.5 |
| | 2 | | 10.0 | -28.2 | 10.9 | -30.9 | | -33.6 | | | 16.1 | -45.7 | 18.5 | -52.5 | 21.1 | -59.7 | 26.7 | -75.6 | | -93.3 |
| | 2 | 100 | 8.9 | -25.5 | 9.7 | -27.8 | _ | -30.3 | 12.4 | - | 14.3 | -41.2 | 16.5 | -47.3 | 18.7 | -53.9 | 23.7 | -68.2 | _ | -84.2 |
| | 3 | 10 | 12.5 | -51.3 | 13.7 12.5 | -56.0 -52.4 | | -61.0 | 17.5 | | 18.5 | -63.1 | 23.3 21.3 | -95.4 -89.2 | 26.5 24.2 | -108.5 | | -137.3 -128.4 | | -169.5 -158.5 |
| | 3 | 50 | 10.0 | -43.5 | 10.9 | -47.6 | | -51.8 | _ | | 16.1 | -70.5 | <u> </u> | -81.0 | 21.1 | -92.1 | | -116.6 | _ | -143.9 |
| | 3 | 100 | 8.9 | -40.2 | 9.7 | -44.0 | | _ | | _ | 14.3 | -65.1 | | -74.8 | 18.7 | -85.1 | 23.7 | | | 132.9 |
| - | 4 | 10 | 21.8 | -23.6 | 23.8 | -25.8 | 25.9 | -28.1 | 30.4 | -33.0 | 35.3 | -38.2 | 40.5 | -43.9 | 46.1 | -50.0 | | -63.2 | 72.0 | -78.1 |
| | 4 | 20 | 20.8 | -22.6 | 22.7 | -24.7 | 24.7 | -26.9 | 29.0 | -31.6 | 33.7 | -36.7 | 38.7 | -42.1 | 44.0 | -47.9 | 55.7 | -60.6 | 68.7 | -74.8 |
| | 4 | 50 | 19.5 | -21.3 | 21.3 | -23.3 | 23.2 | -25.4 | 27.2 | -29.8 | 31.6 | -34.6 | 36.2 | -39.7 | 41.2 | -45.1 | 52.2 | -57.1 | 64.4 | -70.5 |
| | 4 | 100 | 18.5 | -20.4 | | | | | _ | | 30.0 | -33.0 | | -37.8 | 39.2 | -43.1 | 49.6 | -54.5 | | -67.3 |
| I I I I A A | 4 | 500 | 16.2 | -18.1 | 17.7 | -19.8 | _ | | _ | - | 26.3 | -29.3 | | -33.6 | 34.3 | -38.2 | | -48.4 | | -59.8 |
| N. | | 10 | 21.8 | -29.1 | _ | _ | _ | _ | | - | 35.3 | -47.2 | 40.5 | -54.2 | 46.1 | -61.7 | | -78.0 | | -96.3 |
| | 5 | 20 | 20.8 | -27.2 | | | | -32.4 | | - | 33.7 | -44.0 | | -50.5 | 44.0 | -57.5 | | -72.8 | _ | -89.9 |
| | 5 | 50 | 19.5 | -24.6 | | | | - | | | 31.6 | | | -45.7 | 41.2 | -52.0 | | -65.8 | _ | -81.3 |
| | 5 | 100 | 18.5 | -22.6 | 20.2 | | - | -26.9 | _ | -31.6 | | -36.7 | 34.4 | -42.1 | 39.2 | -47.9 | | -60.6 | | -74.8 -59.8 |
| | _ | 500 | 16.2 | -18.1 | 11.1 | -19.8 | 19.3 | -21.5 | 22.7 | -25.2 | 20.3 | -29.3 | 30.2 | -33.6 | 34.3 | -38.2 | 43.5 | -48.4 | 53.7 | -08.8 |

| Compo | nents | and Cl | adding | – Metl | nod 1 | | | | | | | h ≤ 60 ft. | |
|------------|---------|--------|-----------|--------|----------|--------|---------------------|--------|--------------------|--------------------|--------|------------|--|
| igure 30.5 | -1 (cor | t'd) | | Desig | n Win | d Pres | sures | | | | Wall | P. Deefa | Interior Zones |
| Enclos | ed Bui | dings | | | | | | | | | vv an | & Roofs | |
| | | Roo | of Overl | | | | Vind Pi h = 30 f | | e, p _{ne} | ₃₀ (psf |) | | Roofs-Zone 2 / Walls-Zon |
| | | | Effective | | \ | | nd Spee | / | oh) | | | | Roofs - Zone 3 |
| | | | Wind Area | | | | | | | | | | |
| | | Zone | (sf) | 110 | 115 | 130 | 140 | 150 | 160 | 180 | 200 | | |
| | | 2 | 10 | -31.4 | -34.3 | -43.8 | -50.8 | -58.3 | -66.3 | -84.0 | -103.7 | | A A |
| | | 2 | 20 | -30.8 | -33.7 | -43.0 | -49.9 | -57.3 | -65.2 | -82.5 | -101.8 | | |
| | 0 | 2 | 50 | -30.1 | -32.9 | -42.0 | -48.7 | -55.9 | -63.6 | -80.5 | -99.4 | | |
| | lree | 2 | 100 | -29.5 | -32.3 | -41.2 | -47.8 | -54.9 | -62.4 | -79.0 | -97.6 | | |
| | degr | 3 | 10 | -51.6 | -56.5 | -72.1 | -83.7 | -96.0 | -109.3 | -138.3 | -170.7 | | |
| | to 7 | 3 | 20 | -40.5 | -44.3 | -56.6 | -65.7 | -75.4 | -85.8 | -108.6 | -134.0 | | |
| | of 0 | 3 | 50 | -25.9 | -28.3 | -36.1 | -41.9 | -48.1 | -54.7 | -69.3 | -85.5 | | |
| | Roof | 3 | 100 | -14.8 | -16.1 | -20.6 | -23.9 | -27.4 | -31.2 | -39.5 | -48.8 | | |
| | | 2 | 10 | -40.6 | -44.4 | -56.7 | -65.7 | -75.5 | -85.9 | -108.7 | -134.2 | | (Basic 3-sec Gust Wind) |
| | u) | 2 | 20 | -40.6 | -44.4 | -56.7 | -65.7 | -75.5 | -85.9 | -108.7 | -134.2 | | Speed, V _{ult} |
| | ree | 2 | 50 | -40.6 | -44.4 | -56.7 | -65.7 | -75.5 | -85.9 | -108.7 | -134.2 | | |
| | degr | 2 | 100 | -40.6 | -44.4 | -56.7 | -65.7 | -75.5 | -85.9 | -108.7 | -134.2 | | 140 mph |
| | 0 27 | 3 | 10 | -68.3 | -74.6 | -95.3 | -110.6 | -126.9 | -144.4 | -182.8 | -225.6 | | |
| | - 7 to | 3 | 20 | -61.6 | -67.3 | -86.0 | -99.8 | -114.5 | | -164.9 | -203.6 | | Note 3: For hip roofs with $\Theta \leq 25^{\circ}$, |
| | Roof > | 3 | 50 | -52.8 | -57.7 | -73.7 | -85.5 | -98.1 | -111.7 | -141.3 | -174.5 | | Zone 3 shall be treated as Zone 2 |
| | Ro | 3 | 100 | -46.1 | -50.4 | -64.4 | -74.7 | -85.8 | -97.6 | -123.5 | -152.4 | | |

Net Design Wind Pressure, p_{net30} , in lb/ft², for Exposure B at h = 30 ft, V = 140-200 mph

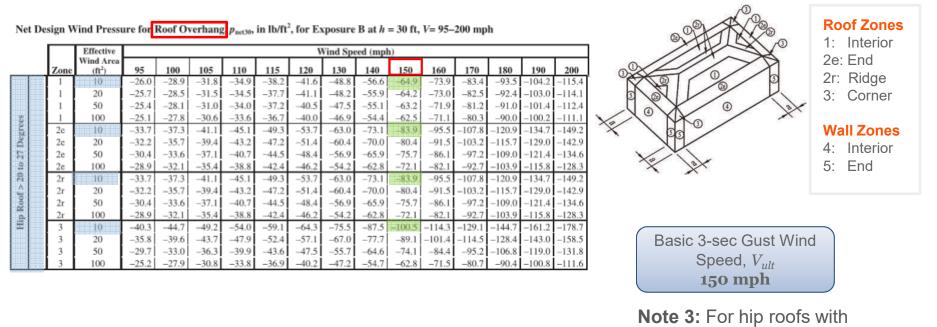
| | | Effective | | | | | | Basi | c Wind | Speed (r | nph) | | | | | |
|------|------|------------------------------------|------|-------|------|-------|------|-------|--------|----------|------|-------|------|-------|------|-------|
| | Zone | Wind Area (ft ²) | 14 | 40 | 1 | 50 | 10 | 60 | 1 | 70 | 18 | 30 | 1 | 90 | 2(| 00 |
| | 4 | 10 | 35.3 | -38.2 | 40.5 | -38.2 | 46.1 | -50.0 | 52.0 | -56.4 | 58.3 | -63.2 | 64.9 | -70.4 | 72.0 | -78.1 |
| | 4 | 20 | 33.7 | -36.7 | 38.7 | -36.7 | 44.0 | -47.9 | 49.6 | -54.1 | 55.7 | -60.6 | 62.0 | -67.5 | 68.7 | -74.8 |
| | 4 | 50 | 31.6 | -34.6 | 36.2 | -34.6 | 41.2 | -45.1 | 46.6 | -51.0 | 52.2 | -57.1 | 58.1 | -63.7 | 64.4 | -70.5 |
| alls | 4 | 100 | 30.0 | -33.0 | 34.4 | -33.0 | 39.2 | -43.1 | 44.2 | -48.6 | 49.6 | -54.5 | 55.2 | -60.7 | 61.2 | -67.3 |
| W | 5 | 10 | 35.3 | -47.2 | 40.5 | -47.2 | 46.1 | -61.7 | 52.0 | -69.6 | 58.3 | -78.0 | 64.9 | -87.0 | 72.0 | -96.3 |
| | 5 | 20 | 33.7 | -44.0 | 38.7 | -44.0 | 44.0 | -57.5 | 49.6 | -64.9 | 55.7 | -72.8 | 62.0 | -81.1 | 68.7 | -89.9 |
| | 5 | 50 | 31.6 | -39.8 | 36.2 | -39.8 | 41.2 | -52.0 | 46.6 | -58.7 | 52.2 | -65.8 | 58.1 | -73.4 | 64.4 | -81.3 |
| | 5 | 100 | 30.0 | -36.7 | 34.4 | -36.7 | 39.2 | -47.9 | 44.2 | -54.1 | 49.6 | -60.6 | 55.2 | -67.5 | 61.2 | -74.8 |

| | | Effective | | | | | | Basic | Wind | Speed (n | nph) | | | | | |
|----------|------|---------------------------------|------|-------|------|-------|------|-------|------|----------|------|--------|------|--------|------|--------|
| | Zone | Wind Area (ft ²) | 14 | 40 | 15 | 50 | 10 | 50 | 17 | 70 | 1 | 80 | 1 | 90 | 2 | 00 |
| | 1 | 10 | 26.3 | -47.2 | 30,2 | 54.2 | 34.3 | -61.7 | 38.8 | -69.6 | 43.5 | -78.0 | 48.4 | -87.0 | 53.7 | -96.3 |
| | 1 | 20 | 22.7 | -41.8 | 26.1 | -48.0 | 29.6 | -54.6 | 33.5 | -61.7 | 37.5 | -69.1 | 41.8 | -77.0 | 46.3 | -85.3 |
| | 1 | 50 | 17.9 | -34.7 | 20.6 | -39.8 | 23.4 | -45.3 | 26.5 | -51.1 | 29.7 | -57.3 | 33.0 | -63.9 | 36.6 | -70.8 |
| Degrees | 1 | 100 | 14.3 | -29.3 | 16.5 | -33.6 | 18.7 | -38.2 | 21.1 | -43.2 | 23.7 | -48.4 | 26.4 | -53.9 | 29.3 | -59.8 |
| 12 | 2e | 10 | 26.3 | -65.1 | 30.2 | 74.8 | 34.3 | -85.1 | 38.8 | -96.0 | 43.5 | -107.7 | 48.4 | -120.0 | 53.7 | -132.9 |
| De | 2e | 20 | 22.7 | -58.2 | 26.1 | -66.8 | 29.6 | -76.0 | 33.5 | -85.9 | 37.5 | -96.2 | 41.8 | -107.2 | 46.3 | -118.8 |
| 27 | 2e | 50 | 17.9 | -49.1 | 20.6 | -56.3 | 23.4 | -64.1 | 26.5 | -72.4 | 29.7 | -81.1 | 33.0 | -90.4 | 36.6 | -100.2 |
| 10 | 2e | 100 | 14.3 | -42.2 | 16.5 | -48.4 | 18.7 | -55.1 | 21.1 | -62.2 | 23.7 | -69.7 | 26.4 | -77.7 | 29.3 | -86.1 |
| 2.0 | 2r | 10 | 26.3 | -65.1 | 30.2 | -74.8 | 34.3 | -85.1 | 38.8 | -96.0 | 43.5 | -107.7 | 48.4 | -120.0 | 53.7 | -132.9 |
| <u>^</u> | 2r | 20 | 22.7 | -58.2 | 26.1 | -66.8 | 29.6 | -76.0 | 33.5 | -85.9 | 37.5 | -96.2 | 41.8 | -107.2 | 46.3 | -118.8 |
| Rool | 2r | 50 | 17.9 | -49.1 | 20.6 | -56.3 | 23.4 | -64.1 | 26.5 | -72.4 | 29.7 | -81.1 | 33.0 | -90.4 | 36.6 | -100.2 |
| | 2r | 100 | 14.3 | -42.2 | 16.5 | -48.4 | 18.7 | -55.1 | 21.1 | -62.2 | 23.7 | -69.7 | 26.4 | -77.7 | 29.3 | -86.1 |
| Hip | 3e | 10 | 26.3 | -65.1 | 30.2 | -74.8 | 34.3 | -85.1 | 38.8 | -96.0 | 43.5 | -107.7 | 48.4 | -120.0 | 53.7 | -132.9 |
| | 3e | 20 | 22.7 | -58.2 | 26.1 | -66.8 | 29.6 | -76.0 | 33.5 | -85.9 | 37.5 | -96.2 | 41.8 | -107.2 | 46.3 | -118.8 |
| | 3e | 50 | 17.9 | -49.1 | 20.6 | -56.3 | 23.4 | -64.1 | 26.5 | -72.4 | 29.7 | -81.1 | 33.0 | -90.4 | 36.6 | -100.2 |
| | 3e | 100 | 14.3 | -42.2 | 16.5 | -48.4 | 18.7 | -55.1 | 21.1 | -62.2 | 23.7 | -69.7 | 26.4 | -77.7 | 29.3 | -86.1 |



 $\Theta \le 25^{\circ}$, Zone 3 shall be treated as Zone 2e and 2r.

Figure 30.4-1 Components and Cladding, Part 2 [h ≤ 60ft (h ≤ 18.3m)]: Design Wind Pressure for Enclosed Buildings – Walls and Roofs



Note 3: For hip roofs with $\Theta \le 25^\circ$, Zone 3 shall be treated as Zone 2e and 2r.

Figure 30.4-1 Components and Cladding, Part 2 [$h \le 60$ ft ($h \le 18.3$ m)]: Design Wind Pressure for Enclosed Buildings – Walls and Roofs

Results Comparison

| | | Roof Pressures (ps | n | Wall Press | sures (psf) | Roof Pressures w/ Overhangs (psf) | | | |
|---------------------|-------|--------------------|-------|------------|-------------|-----------------------------------|-------|-----|--|
| Zone – ASCE 7-10 | 1 | 2 | 3 | 4 | 5 | 1 | 2 | 3 | |
| P _{net30} | 20.3 | 20.3 | 20.3 | 35.3 | 35.3 | 20.3 | 20.3 | 20. | |
| | -32.3 | -56.2 | -56.2 | -38.2 | -47.2 | -32.3 | -65.7 | -65 | |
| P _{net} | 29.8 | 29.8 | 29.8 | 51.7 | 51.7 | 29.8 | 29.8 | 29. | |
| | -47.5 | -82.6 | -82.6 | -56.2 | -69.4 | -47.5 | -96.6 | -96 | |

| | | Roof Pre | essures (psf |) | Wall Pres | sures (psf) | Roof Pressures w/ Overhangs (psf) | | | | |
|---------------------|-------|----------|--------------|--------|-----------|-------------|-----------------------------------|--------|--------|--------|--|
| Zone – ASCE 7-16 | 1 | 2e | 2r | 3 | 4 | 5 | 1 | 2e | 2r | 3 | |
| P _{net30} | 30.2 | 30.2 | 30.2 | 30.2 | 40.5 | 40.5 | 30.2 | 30.2 | 30.2 | 30.2 | |
| | -54.2 | -74.8 | -74.8 | -74.8 | -38.2 | -47.2 | -64.9 | -83.9 | -83.9 | -83.9 | |
| P _{net} | 44.4 | 44.4 | 44.4 | 44.4 | 59.5 | 59.5 | 44.4 | 44.4 | 44.4 | 44.4 | |
| | -79.7 | -110.0 | -110.0 | -110.0 | -56.2 | -69.4 | -95.4 | -123.3 | -123.3 | -123.3 | |

Things To Go Do





Bookmark the following websites:

- Free I-Codes: https://codes.iccsafe.org/public/collections/l-Codes
- ATC Wind Speed by Location: <u>http://hazards.atcouncil.org/</u>



Go check out the *High-Performance Solutions for High-Wind Forces* microsite <u>www.strongtie.com/hw</u>



Simpson Strong-Tie

Changes in Wind Design with ASCE 7-16

THANK YOU!

For a library of **Simpson Strong-Tie** AIA CES courses, visit http://www.strongtie.com/workshops

