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Foundation Design Challenges for Basements in Saturated Coastal Plains



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ASCE Palm Beach Chapter
Lantana, August 9, 2022




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Foundation Design Challenges for Basements in Saturated Coastal Plains

Content

- GEOTECHNICAL PARAMETERS AND SOIL PROFILE
- FOUNDATIONS FOR BUILDINGS WITH BASEMENTS
 - Excavations and GWT
 - Intermediate Foundations/Ground Improvement
 - GWT Handling - Dewatering
 - Uplift Pressure Control
 - Geo Construction Approach
- CONCLUSIONS

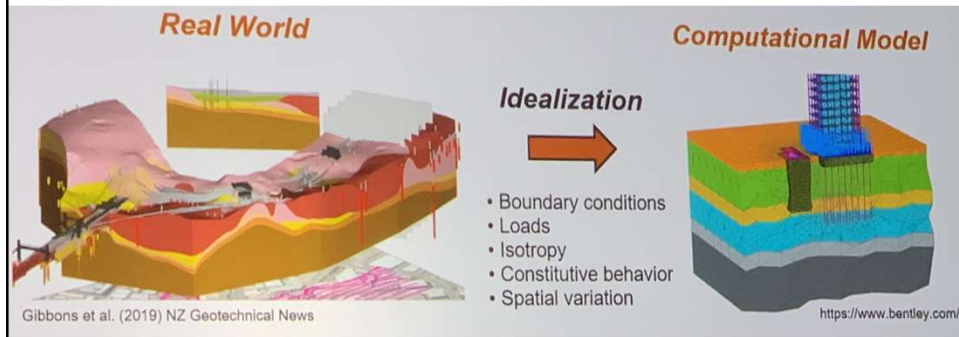


Professor George F. Sowers
1921 - 1996



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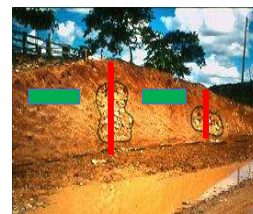
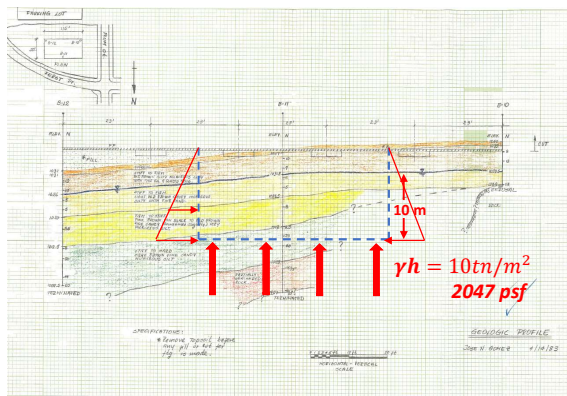
Geotechnical Parameters and Soil Profile



This is Our Challenge!

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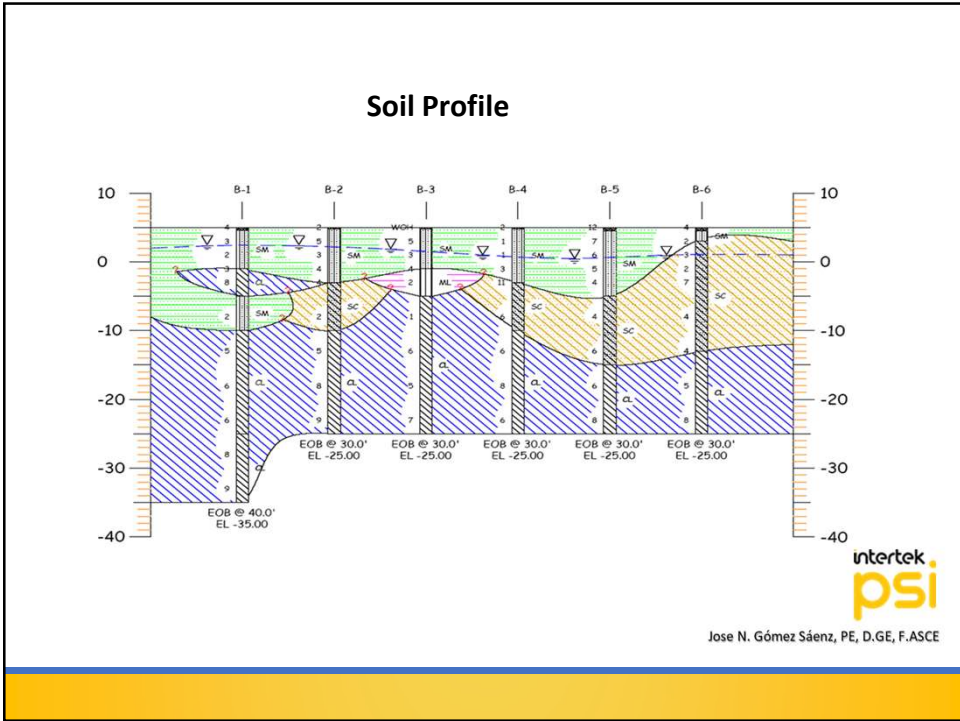
Geotechnical Parameters and Soil Profile Significant Challenges



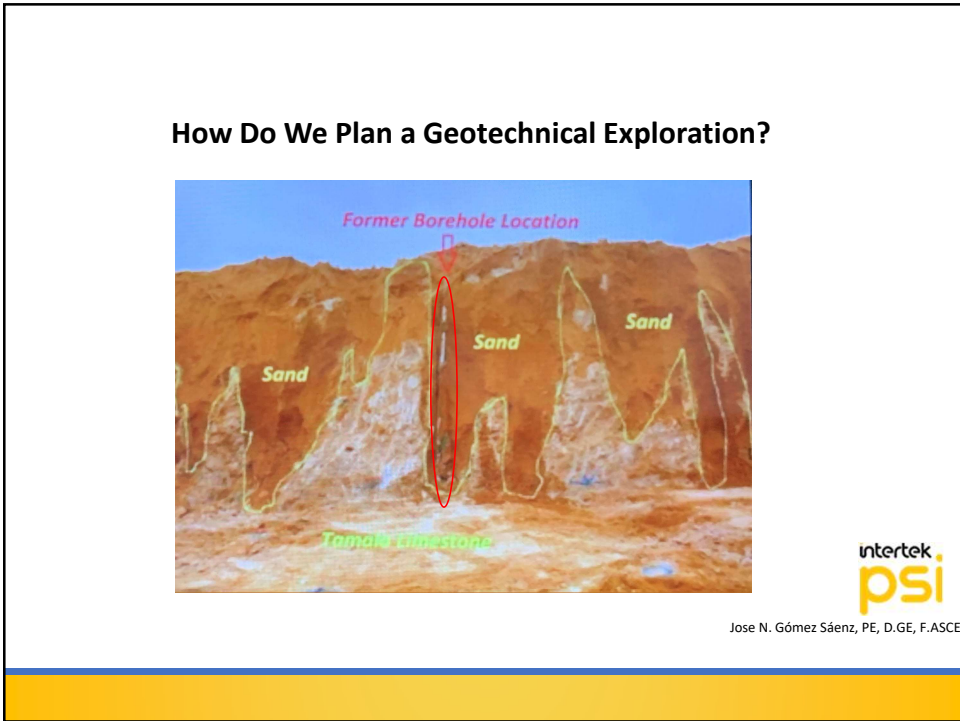
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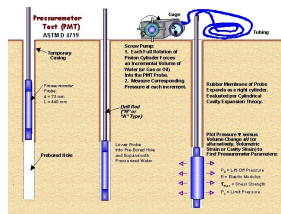
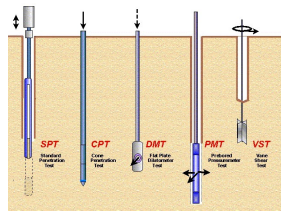


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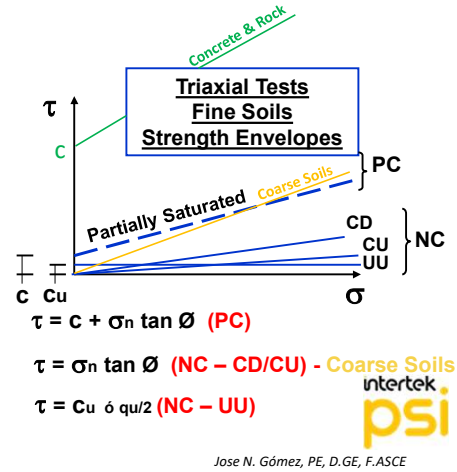


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Geotechnical Parameters and Soil Profile



<http://www.geotechdata.info/geotest/cone-pressuremeter-test.html>



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Figure 5-2: Bearing Capacity Failure of Silo Foundation
(Vesic, 1975, from Tschebotarioff, 1951)

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Professor Ralph B. Peck

Less is More ...

“If you can’t reduce a difficult engineering problem to just one 8-1/2 x 11 sheet of Paper, you will probably never understand it.” - Peck

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CE 484

GEOTECHNICAL CASE HISTORIES

A typical 1-page summary sheet prepared by students enrolled in Ralph Peck's Geotechnical Case Histories course (in this case, the student was NGI's Elmo DiBiagio).

Students would be presented information as though they were consultants engaged in providing services on a project. The briefing would include the type of information normally known at the beginning of a job. From that point on, the students were required to ask questions, in order to elicit additional information needed to make engineering assessments.

If you cannot reduce a difficult engineering problem to just 8 1/2 x 11-inch sheet of paper, you will probably never understand it. Ralph B. Peck

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Building Foundations- Excavations and GWT

Ideal Conditions? ??



https://www.skypumpsest.com/page_english.php?id=2



<https://www.groundwatereng.com/blog/2016/03/dewatering-for-basement-construction>



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Hussin, Baquerizo and Cook, "Basements On The Beach", ASCE-GEOSTRATA, July/August 2019



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6/10/2022

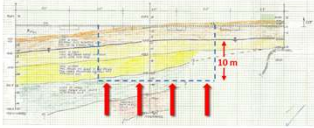
475 Royal Palm

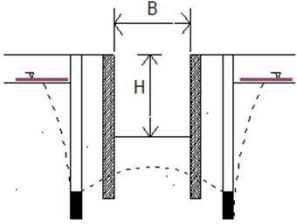


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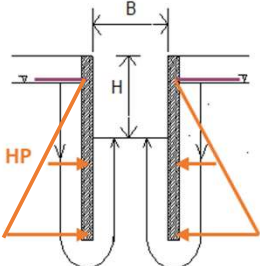
GWT Handling – Dewatering in Granular Soils

Problem: -Soils with medium to high permeability.
 -Seepage needs to be controlled to reduce hydrostatic pressure (HP) and uplift force (UF) at excavation bottom.






Well Points / Deep Wells



**Deep Wall
(Reduce Hyd. Gradient)**



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Dewatering System Design

Design Outline

- Soil Profile Definition (o.k)
- Soil Parameters Evaluation and Soil Classification (o.k)
- Aquifer(s) Characterization (o.k)
- Coefficient of Permeability (K, cm/sec) Evaluation
 - Pumping Test
 - Amoozemeter Test
 - Correlations (Grain Size – Sands)
- Dewatering System Alternatives and Selection
 - Conventional Well Points
 - Deep Wells
 - Eductor Wells



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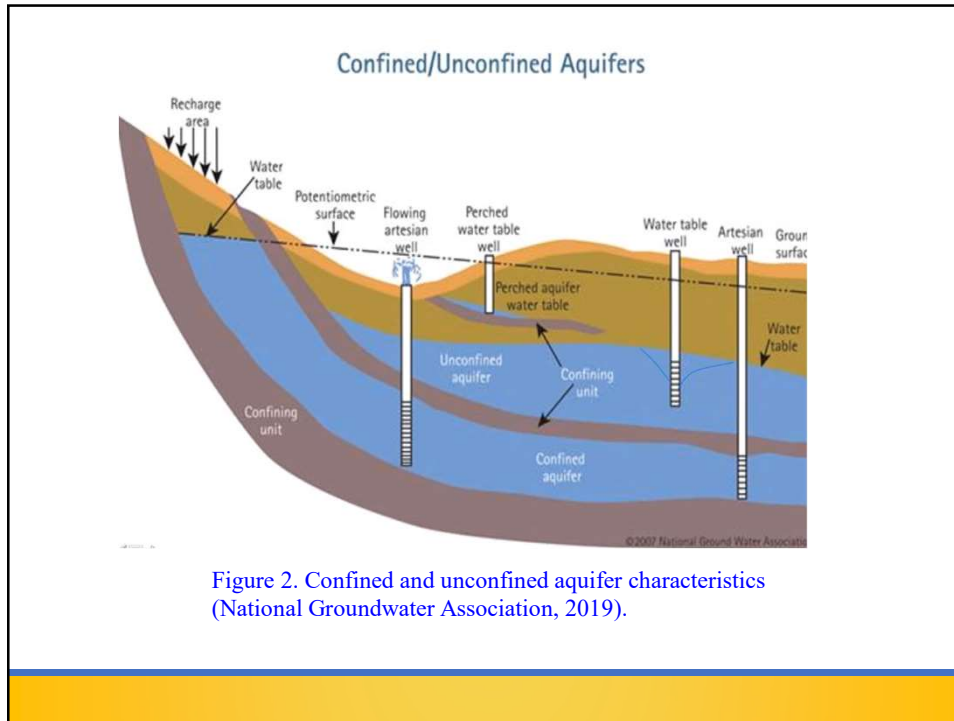


Figure 2. Confined and unconfined aquifer characteristics (National Groundwater Association, 2019).

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Estimation of Total System Discharge Capacity

Drawdown Flow Computation Clay at 8 Mt BGS (26.2 FEET BGS)											Project No.		Observations	
H(ft)	ho(ft)	Wexc	Lexc	ro	R(ft)	k cm/sec	k ft/min	A=(H-ho)	B=(H+ho)	C=(R+ro)	D=(R-ro)	Q ft ³ /min		Q gpm
18.5	5	125	200	89	300	0.00092	0.0018	13.5	23.5	389	211	1.67	12	IHA-1
18.5	5	125	200	89	300	0.00553	0.0109	13.5	23.5	389	211	10.01	75	IHA-2
18.5	5	125	200	89	300	0.00018	0.0004	13.5	23.5	389	211	0.33	2	IHA-3
18.5	5	125	200	89	300	0.00435	0.0086	13.5	23.5	389	211	7.87	59	Average In Situ Perms
18.5	5	125	200	89	300	0.0075	0.0148	13.5	23.5	389	211	13.57	102	Pumping Test
18.5	5	125	200	89	300	0.00486	0.0096	13.5	23.5	389	211	8.80	66	Average All
Well Formula														
18.5	5	125	200	89	300	0.00435	0.0086	0.026895	317.25	3.36	0.53	7.04	53	Average In Situ Perms
18.5	5	125	200	89	300	0.0075	0.0148	0.04637	317.25	3.36	0.53	12.14	91	Pumping Test
18.5	5	125	200	89	300	0.00486	0.0096	0.030048	317.25	3.36	0.53	7.87	59	Average All

$Q=1.57k(A*B*C)/D$ "Darcy's law formula"
 k=cm/sec x 1.968 to get ft/min
 Units: ft³/min, x 7.5 to get gpm
 H= Aquifer Thickness (ft)
 ho= Drawdown (ft)-From the bottom of the aquifer
 Wexc= Width of Excavation (ft)
 Lexc= Length of Excavation (ft)
 ro= Average radius of exc. bottom
 (SGRT W*L/m) - ft
 k= Coefficient of Permeability (cm/sec)

Note: This analytical method allows to estimate the approximately flow (Q) required to dewatering a site with geometry W x L, and drawdown ho.

Ref.: Ground Control and Improvement, Petros P. Xanthakos, et al. 1994 (Wiley)

NOTES:

1. Total System Capacity: 65 gpm
2. Single WP or Eductor Capacity: 1.0 gpm
3. Total System Length: 650 ft (200'x125')
4. Minimum WPs or Eductors Required: 65 units @ 10' centers

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Poor Dewatering Outcome



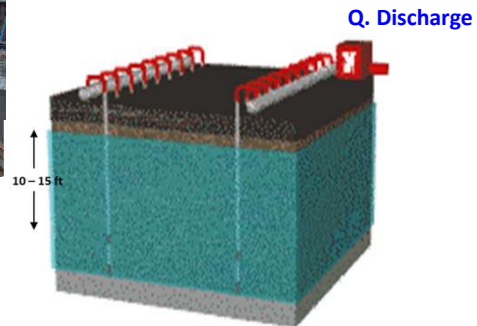
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Well Point and Sheet Pile Wall Systems



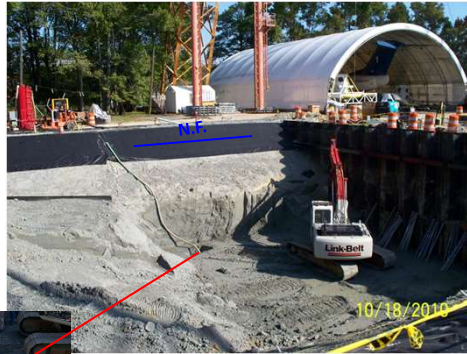
GWT-Drawdown Simulation



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Well Point and Sheet Pile Wall Systems

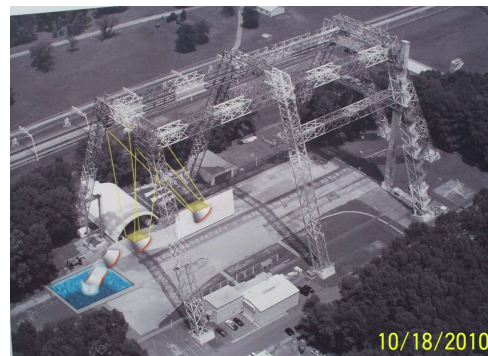
NASA Gantry Impact Basin - 2014



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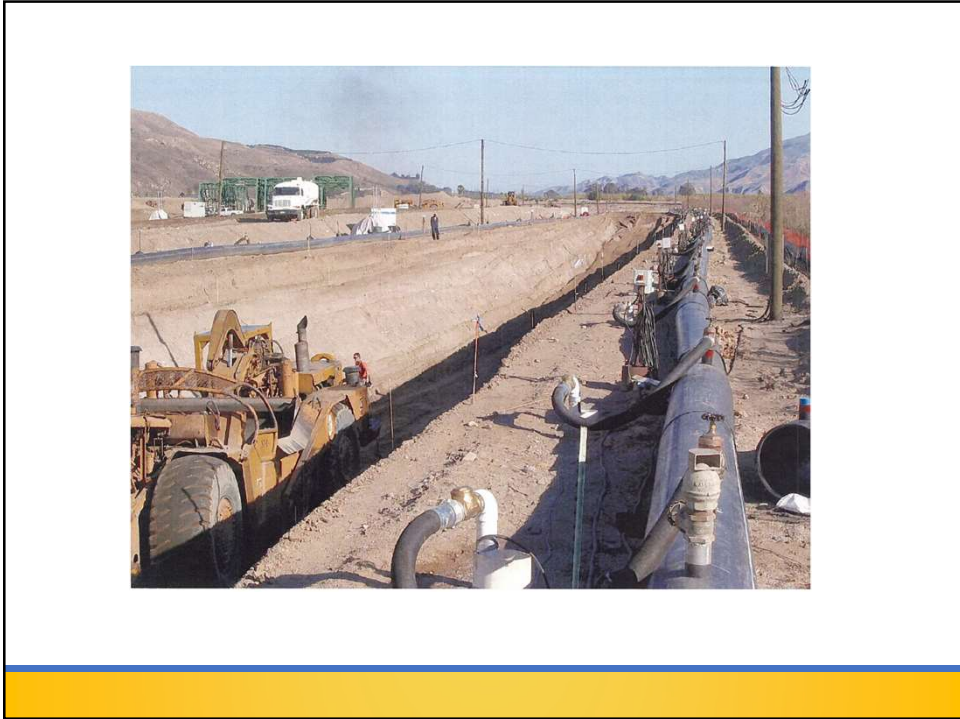
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NASA Gantry Impact Basin - 2014



<https://www.nasa.gov/centers/langley/exploration/hib.html>

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SPW-Design Considerations

Diagram illustrating trench cross-section parameters: ϕ and $c = 0$, $\phi = 0$, $c = 0$. Labels include Design Line, Sand, and various dimensions like P_1 , P_2 , P_3 , P_4 , P_5 , P_6 , P_7 , P_8 , P_9 , P_{10} , P_{11} , P_{12} , P_{13} , P_{14} , P_{15} , P_{16} , P_{17} , P_{18} , P_{19} , P_{20} , P_{21} , P_{22} , P_{23} , P_{24} , P_{25} , P_{26} , P_{27} , P_{28} , P_{29} , P_{30} , P_{31} , P_{32} , P_{33} , P_{34} , P_{35} , P_{36} , P_{37} , P_{38} , P_{39} , P_{40} , P_{41} , P_{42} , P_{43} , P_{44} , P_{45} , P_{46} , P_{47} , P_{48} , P_{49} , P_{50} .

"DULL MEND" JANG 7/9

EARTH SUPPORT METHOD

SEE PAGE 190. as a complement.

NON-COHESSIVE SOIL

IF NO DRAINAGE

RESULTANT PRESSURE ($P_p - P_u$)

$P_p = \text{Surcharge} + \text{Soil}$

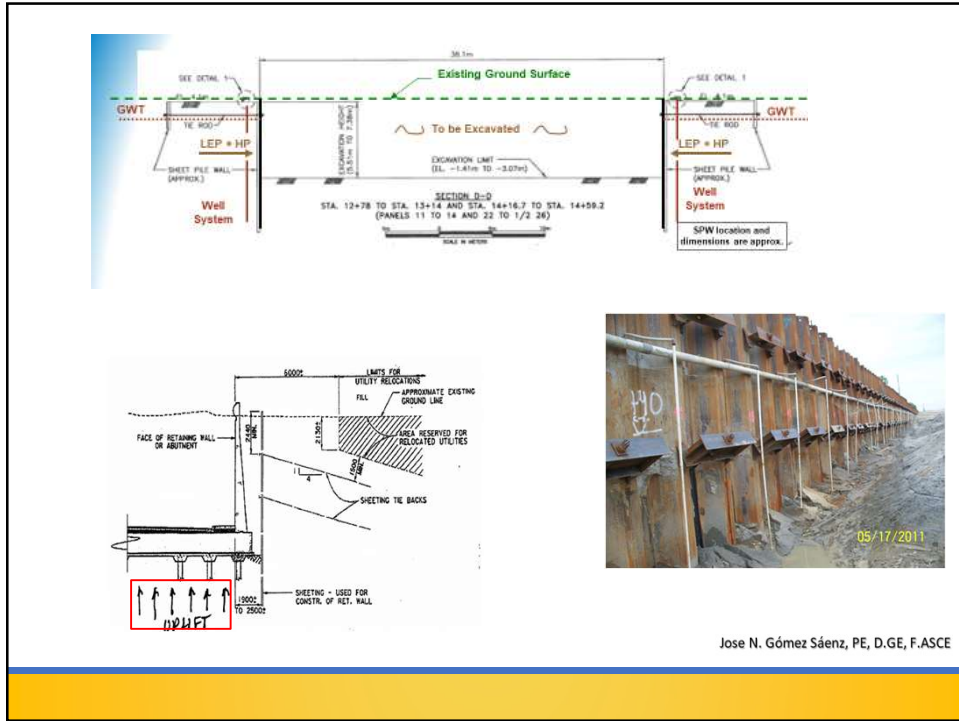
$\textcircled{0} \sigma_v = \sigma'_v z'$
 $\sigma'_h = k_a \sigma'_v$

$\textcircled{0} \bar{\sigma}_v = \sigma_{v0} + (\gamma - \gamma_w)h$
 $\bar{\sigma}_h = \bar{\sigma}_v k_a$

Client: American Infrastructure	
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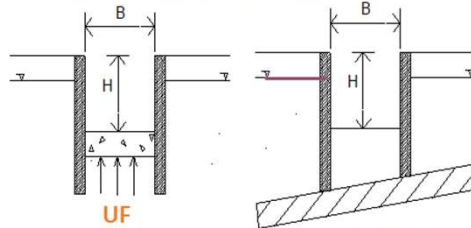
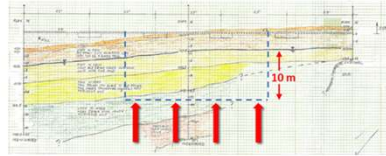
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When Things Go South



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GWT Handling – Controlling Uplift Forces in Granular Soils



Bottom/Basement Slab Resists Uplift Force

Check for Aquifer Walls Embedded in Impervious Layer



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Case History of 15-Meter Deep Vault Excavation

"Excavación cajón como estructura para el manejo de carbón: diseño, construcción y comportamiento". XI Jornadas Geotécnicas de la Ingeniería Colombiana (SCI), 2001.

17 Deep Wells

VIGA CAREZAL
VIGA PERIMETRAL INTERMEDIA
VIGA CINTURON
CODAL EN CONCRETO
 15 m

6.5 – 10.0 lt/sec
 12,000 m³/day; 85K People

CONEXIONES (Legenda)
 ● PISO DE BOMBA
 ○ PISO DE BOMBEO
 C.S. CONCRETO ARMADO
 → TUBERIA CONCRETO PARA BOMBEO
 → TUBERIA DE BOMBEO

Panela prefabricada
Viga perimetral intermedia

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**Ground Improvement
Soil Mixing Plug Construction**

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Hussin, Baquerizo and Cook, "Basements On The Beach", ASCE-GEOSTRATA, July/August 2019

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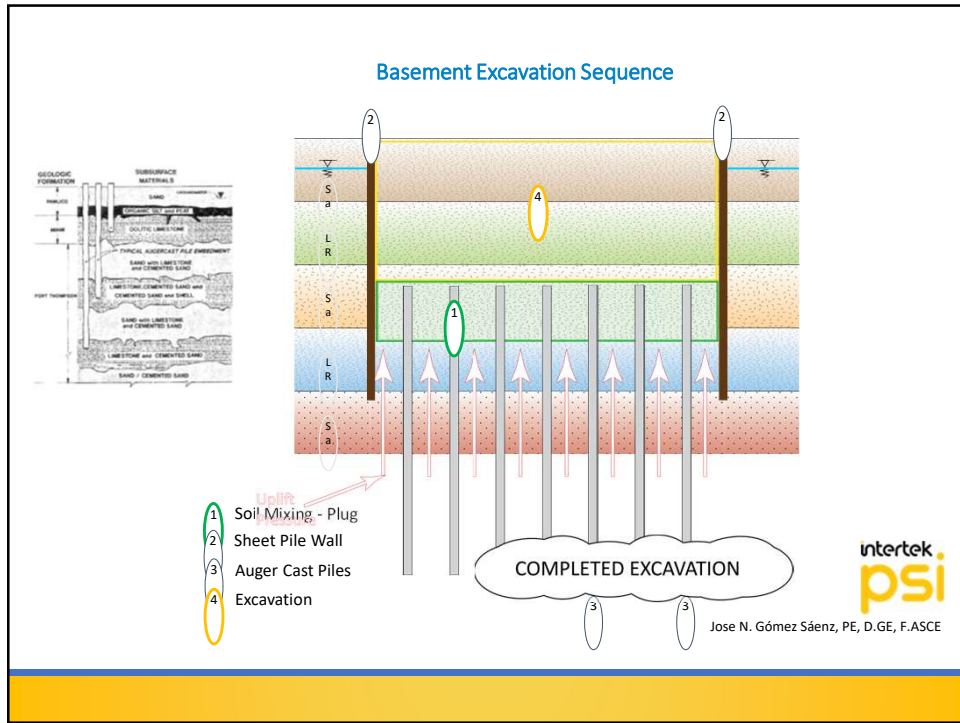
Generalized Stratigraphy of South Florida

AUGERCAST PILES - SOUTH FLORIDA EXPERIENCE
By Rudolph P. Frizzi, P.E. and Matthew E. Meyer, P.E.
Members, ASCE. (2000)

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Conclusions

- When High GWT and Granular Soils with high permeability, hydrostatic uplift pressures are a geotechnical and structural problem.
- GWT drawdown systems could be impractical in situations with presence of adjacent structures.
- Soil mixing plugs together with an appropriate perimetric pre-excavated wall creates a “bathtub” structure supported with piles to control uplift pressure, as an option in coastal plain geologies.



Thank You

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